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RESPOND – FAULT CURRENT LIMITING SERVICE SAFETY JUSTIFICATION

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RESPOND -FAULT CURRENT LIMITING SERVICE JUSTIFICATION

Electricity North West Ltd

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WSP Manchester Technology Centre Oxford Rd, M1 7ED Manchester

Tel: +44 (0) 161 200 5000

www.wsp.com



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Authorised by	P Yadav			
Signature	Tanhog Gadav			
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PRODUCTION TEAM

CLIENT

Innovation Engineer	Kieran Bailey
Innovation Delivery Manager	Paul Turner
WSP	
Project Manager	Pankaj Yadav
Technical Specialist	Peter Watson
Safety Specialist	Mike Irwing
Project Engineer	Gerasimos Doris

GLOSSARY

1001	One out of One
1002	One out of Two
ALARP	As Low As Reasonably Practicable
AP	Adaptive Protection
BM	Balancing Mechanism
СВ	Circuit Breaker
СТ	Current Transformer
DC	Direct Current
DNO	Distribution Network Operator
ENA	Energy Networks Association
ETA	Event Tree Analysis
FCL	Fault Current Limiting
FLAT	Fault Level Assessment Tool
FLMT	Fault Level Mitigation Technique
HAZOP	Hazard and Operability
HV	High Voltage
HSE	Health and Safety Executive
H&S	Health and Safety
IPCT	Interposing Current Transformer
LCNF	Low Carbon Network Fund
LV	Low Voltage
NAFIRS	National Fault and Interruption Reporting Scheme
NMS	Network Management System
Ofgem	Office of Gas and Electricity Markets
OHL	Overhead Line
QRA	Quantitative Risk Assessment
SDRC	Successful Delivery Reward Criteria
SFAIRP	So Far As Is Reasonably Practicable
SHE	Safety Health and Environment
SIL	Safety Integrity Level
SIPS	System Integrity Protection Scheme

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EXECUTIVE SUMMARY

Electricity North West's Respond project is trialling new methods of mitigating fault level issues as alternatives to expensive replacement of equipment. The Respond project is a Low Carbon Network Fund (LCNF) Tier 2 project, which is funded by the Low Carbon Innovation Fund.

One of these methods is Fault Current Limiting (FCL) which uses protection relay functionality at customer sites to protect 11kV substations where potential fault levels exceed equipment ratings at the substation. FCL service works by sensing a fault current at the customer site and shedding the customer generator or machine load to limit potential fault current before the substation circuit breaker is opened to clear the fault as normal. This prevents equipment ratings being exceeded and provides safe operation of equipment.

This safety justification is required to satisfy the LCNF project's Successful Delivery Review Criteria. It has been produced by WSP, independently from Electricity North West, with input from and peer review by other DNO(s) and presented to HSE to demonstrate that a robust approach has been taken.

A safety assessment has been undertaken to develop this safety justification for the implementation of the defined FCL scheme within the Electricity North West network. Key outcomes of the safety assessment are summarised below.

The safety assessment has categorised substation sites as low, medium or high risk in order to assign a range of measured safety requirements. In simple terms, low risk sites are rural and not densely populated, medium risk sites are typical urban locations and high risk sites are in continuously busy, densely populated areas. The analysis has shown that, based on arguably conservative assumptions, it would be acceptable from a safety viewpoint to fit substations with an FCL system provided that they are low risk sites and not medium or high risk sites. The FCL system would be required to meet the Safety Integrity Level 2 (SIL2) requirements of BS EN 61508.

The safety assessment process has determined four hazard scenarios presenting the most significant risk. These are:-

- a) Short circuit of the busbar in a substation resulting in excessive fault current
- b) Short circuit within a Circuit Breaker in the substation resulting in excessive fault current
- c) Short circuit of the feeder cables or something connected to these cables such that the feeder cable withstand current is exceeded
- d) Short circuit of the overhead line or something connected to the overhead line such that the overhead line withstand current is exceeded

These hazards only represent a hazard to personnel if the fault energy is not adequately contained and results in effects such as ground disruption due to cable failure, overhead line conductors clashing and falling to the ground, or fire and structural damage to substations. In these cases the hazards could potentially result in injuries and fatality to workers and members of the public.

Safety requirements have been established (further to those already in place for the existing network and operations) which would ensure control of the risk associated with each of these scenarios to a 'Tolerable' level. The safety requirements include:

- Application conditions that must be satisfied before applying FCL service to a site, i.e. pre-requisites
- b) Safety function and performance measures necessary for the FCL system, including safety integrity level
- c) Implementation, operating and maintenance measures necessary to control safety risk of the FCL scheme in use, including compliance with safety management systems, standards, procedures and codes of practice.

The study has also reviewed the requirements laid down by the health and safety applicable legislation. This identified 'absolute' requirements of the Electricity At Work (EAW) Regulations, specifically Regulations 5, 11 and 12 which, unlike other legislation requirements, are not satisfied by 'reasonably practicable' risk control measures and safety arguments. The EAW Regulations, Regulation 29, sets out the means for a legal defence in the event these 'absolute' regulations are breached.

This point has been discussed with HSE and the HSE's view was that provided a risk assessment had been performed which justified that the risk presented by the FCL scheme was 'Broadly Acceptable' then this would support an Electricity North West claim that it had taken sufficient steps to comply with the Regulations.

It should be noted that amongst the requirements for application of FCL it is necessary that the busbar itself and the feeder circuit breakers are able to withstand the fault currents that will occur up until the point at which FCL is operates (approximately 400ms). Ability to meet this condition has not yet been demonstrated by the FCL development team but is a clear pre-requisite for application of the FCL service.

1 INTRODUCTION

1.1 INTRODUCTION

Electricity North West () commissioned WSP to assess the safety of the three Fault Level Mitigation (FLM) techniques being trialled by their Respond project and to assess compliance of the techniques with the relevant UK legislation.

WSP has prepared this Safety Justification independently as part of an unbiased and robust approach to assess the safety of the Respond FLM techniques.

1.2 THE RESPOND PROJECT

The prospective amount of current that will flow in an electrical network when a short circuit fault occurs is referred to as the fault level and it is an important parameter in the definition of power equipment capabilities. Network fault levels are increasing above the rating of some existing equipment due to the connection of distributed generation and changes in network topology.

Electricity North West''s Respond project¹ is trialling new methods of mitigating fault level issues as alternatives to expensive replacement of equipment. The Respond project is a Low Carbon Network Fund (LCNF) Tier 2 project, which is funded by the Low Carbon Innovation Fund. Comprehensive project information can be obtained from the Respond website.

The Respond project aims to demonstrate the use of three innovative FLM techniques which have not been previously used by a Distribution Network Operator (DNO) in the UK, namely;

- Is Limiters (essentially an extremely fast acting switch and fuse device which senses the fault current rise and reconfigures the circuit so as to reduce the fault current)
- Adaptive Protection (AP) (a system whereby one out of two transformers in a substation is rapidly disconnected so as to reduce the subsequent fault current so that by the time other circuit breakers trip they will not see excessive current)
- Fault Current Limiting service (FCL service) (a system whereby an external customer's site that contains generators or motors that could act as a fault current feed is rapidly disconnected so as to reduce the subsequent fault current so that by the time other circuit breakers trip they will not see excessive current)

1.3 REQUIREMENT FOR SAFETY JUSTIFICATION

The FLM techniques being trialled by the Respond project, including FCL service, can introduce changes to the way existing equipment is operated. A safety justification assesses the changes to provide a clear and comprehensive argument that the proposed application of each FLM technique is or is not acceptably safe.

The Respond project's safety justifications are required to satisfy the Successful Delivery Review Criteria, SDRC 9.3.8, as detailed below:

¹ http://www.Electricity North Westl.co.uk/respond/about-respond/what-is-respond-

Criteria	Evidence
Write Safety Case for each fault level mitigation technology deployed	Publish peer reviewed Safety Cases on the Respond project website by September 2018

The SDRC uses the term 'safety case'. The Health and Safety Executive (HSE) views a safety case as a document associated with a licensing requirement to do work, such as in the nuclear industry. The HSE review such safety cases and may grant approval. In these terms, a safety case is not necessary for the use of the Respond project's FLM techniques because the techniques are not licensed and HSE permission does not need to be granted. However, Electricity North West are committed to safety and as part of their safety processes they will produce a safety justification for the approach and this is presented here in the form of a safety case even though it is not part of a licence requirement.

Safety justifications for the Respond project have been produced by WSP, independently from Electricity North West, with input from and peer review by other DNO(s) and presented to HSE to demonstrate that a robust approach has been taken.

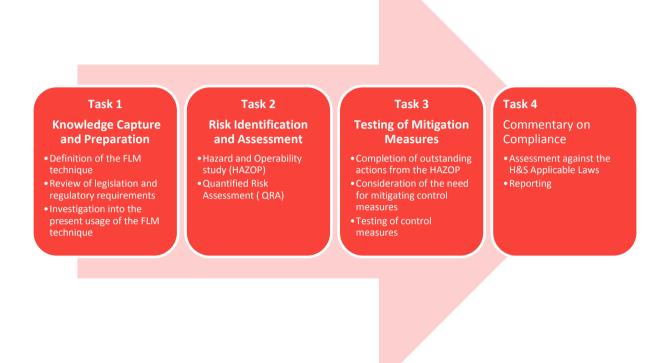
Three safety justifications will be prepared by WSP, one for each of the three FLM techniques being trialled by the Respond project, to assess their safety and compliance with Applicable Laws insofar as these Applicable Laws relate to health and safety (H&S Applicable Laws).

This safety justification report covers the Fault Current Limiting (FCL) FLM technique. This safety justification is concerned with the safety of people, including the general public, through operation and maintenance. It does not specifically address the other aspects of the lifecycle (e.g. the manufacture, storage and disposal of the devices) or other risk categories (environmental, asset, reputation, etc.). It does not address failure to supply (i.e. compliance with Electricity North West's Electricity Distribution Licence) or the environmental impact of incorrect operation.

The I_{S} Limiter technique and the Adaptive Protection FLM technique are addressed in separate reports.

1.4 SAFETY JUSTIFICATION PROJECT

Figure 1-1 depicts the tasks undertaken to complete the safety assessment project.





1.5 REPORT STRUCTURE

This report describes the process that has been followed to assess the safety of the use of FCL service in distribution networks and presents the results along with the conclusions and implications arising from those results. It comprises the following sections;

- Section 1 this introduction, provides the scope of the study and overview of the report structure;
- Section 2 describes the safety assessment methodology that has been followed;
- Section 3 defines FCL service for the purpose of this safety assessment;
- Section 4 explains the tolerability of risk framework and derivation of targets for this FCL scheme
- Section 5 provides details of the review of applicable health and safety laws undertaken;
- Section 6 details results and findings of the hazard identification and quantified risk assessment with discussion of results, comparison with requirements and sensitivity to changes;
- Section 7 draws out conclusions and the implications of the safety assessment and suggests further steps in the development of an FCL scheme.

Appendices present detail from analysis, including hazard list, QRA and safety requirements

2 SAFETY ASSESSMENT APPROACH

A review undertaken at the start of this study has not revealed evidence of previous applications of an FLM technique either very similar or identical to FCL in the UK and elsewhere. Consequently, no previous safety justification exists for this type of application and no precedent exists for reference or development.

However, the approach to assessment and justification of safety related systems generally is well understood and has been adopted for this study. This section describes the approach and the steps taken, as outlined in Figure 2-1, including wider management and supporting activities to ensure the quality and completeness of the final safety justification.

2.1 REVIEW OF LEGISLATION AND REGULATORY REQUIREMENTS

The first step of the assessment determines the legislative and regulatory framework applying to FCL service. This defines constraints and key requirements, which FCL service must comply with. The remaining steps in the safety assessment approach are tailored to address these requirements.

For most safety related applications, the most relevant legislation is the Health and Safety at Work Act 1974² (HSW Act) which adopts a risk based approach, specifying that risks should be reduced So Far As Is Reasonably Practicable (SFAIRP). This essentially means weighing the risk presented by an FCL installation against the trouble, time and money needed to control that risk. Thus, FCL risks would be expected to be controlled SFAIRP.

Other legislation applies to the use of FCL service, such as the Electricity at Work Regulations (EAWR) 1989. This legislation includes requirements which are absolute rather than risk based. For example, EAWR Regulation 5 requires that no electrical equipment shall be put into use where its strength and capability may be exceeded in such a way as may give rise to danger. If FCL service is applied in a scenario where the fault current would exceed the circuit breaker rating, should the FCL service fail, then it could be interpreted that this is in contravention of Regulation 5.

Therefore, in conducting a review of the legislation and regulatory requirements, it is essential to consult with other industry stakeholders and particularly with HSE to establish their view as to the requirements arising from applicable H&S Laws and whether FCL service can meet those requirements.

Findings of the review of H&S applicable laws are presented and discussed in Section 5.

2.2 ESTABLISHING RISK CRITERIA

In order to determine whether the application of FCL service presents a 'Broadly Acceptable' or 'Tolerable' risk in accordance with legislation (SFAIRP and As Low As Reasonably Practicable (ALARP) principles) it is necessary to establish appropriate risk tolerability criteria.

² http://www.legislation.gov.uk/ukpga/1974/37/contents

The study has investigated industry practice, consulted with Electricity North West and used guidance from HSE's 'Reducing Risk Protecting People' publication to establish appropriate risk criteria for use with the Respond project.

Findings are presented and discussed in Section 4.

2.3 SAFETY ASSESSMENT METHOD

The safety justification considers safety, health and welfare issues associated with the use or failure of the FLM technique and preparation of a critical risk assessment. It is based on the specific application of the FLM technique which was developed for proposed trials and extrapolates to consider some options for implementation.

The overall process is summarised in Figure 2-1 below and each stage of the process is then briefly described.

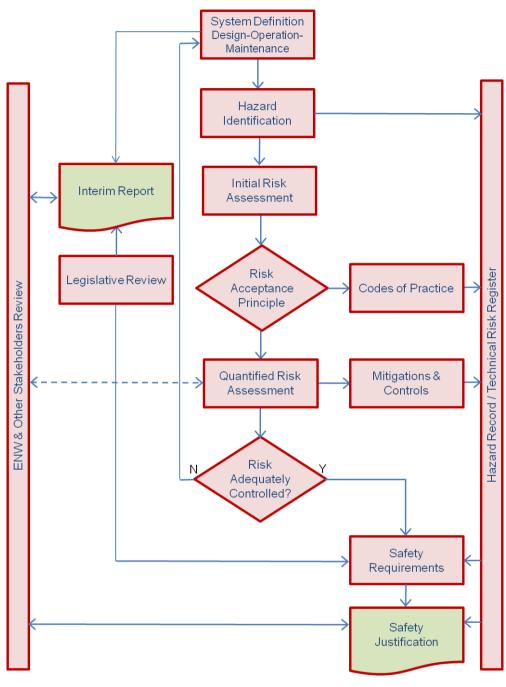


Figure 2-1 Respond Project Safety Assessment Process

2.4 SYSTEM DEFINITION

The system definition (Section 3) was based on a reference system with a number of alternatives. This formed the basis for the remainder of the analysis.

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2.5 HAZARD IDENTIFICATION

A Hazard and Operability (HAZOP) workshop was conducted for FCL service based on the reference system described in Section 3. Identified hazards are presented in Section 6.1 with further detail in Appendix A.

2.6 INITIAL RISK ASSESSMENT

An initial risk assessment was conducted during the HAZOP and was based on the engineering judgement of those present regarding frequency and consequence of the hazards.

2.7 RISK ASSESSMENT PRINCIPLE

Where a particular risk can be controlled purely by adherence to existing standards or regulations the "code of practice" principle was used. Where such a code of practice did not exist, the Quantified Risk Assessment (QRA) principle was used.

2.8 CODES OF PRACTICE

Where codes of practice were applicable, they were identified and conformance to them became the justification for safety.

2.9 QUANTIFIED RISK ASSESSMENT

Risk associated with some hazards could not be satisfactorily controlled through the application of codes of practice. Therefore, in these cases a quantified risk assessment (QRA) has been undertaken. The QRA has determined where further control measures have been required to satisfactorily reduce that risk. The QRA and its findings are presented and discussed in Sections 6.2 to 6.5 with supporting calculations at Appendix B.

2.10 SAFETY REQUIREMENTS

Results from the HAZOP and QRA and from review of the H&S applicable laws have determined safety requirements and conditions necessary for the application of FCL service.

The safety justification includes statements and evidence to support where each safety requirement is achieved by the implementation of FCL service defined in Section 3. The safety justification also suggests improvements to the defined FCL service where this is necessary to achieve a safety requirement.

Safety requirements arising from the HAZOP and QRA are discussed in Section 6.7 and presented in Appendix C.

2.11 PROJECT SAFETY ORGANISATION

The project safety organisation depicts Electricity North West's role as owner of the safety justification, WSP as independent producer of the safety justification and the involvement of other stakeholders in the consultation and review process, as shown in Figure 2-2.

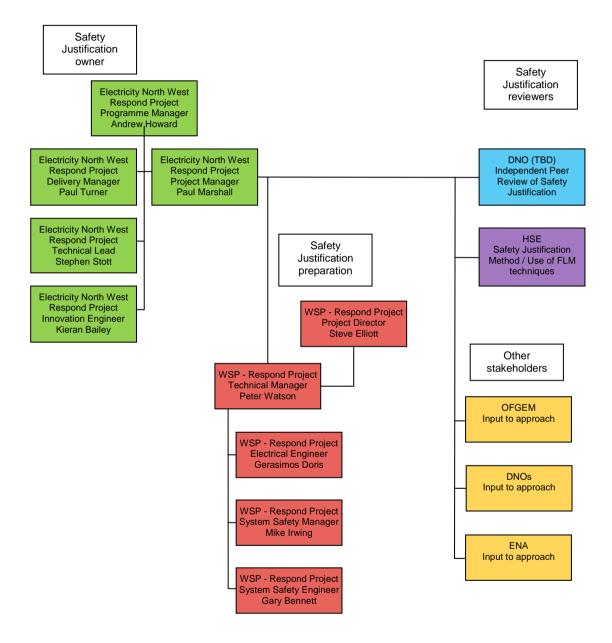


Figure 2-2 Safety Justification delivery and responsibility organisation

2.12 MANAGEMENT, REVIEW AND APPROVAL

The study has been undertaken in stages with interim findings being presented, documented and reviewed incrementally to ensure quality and validity of input data, assumptions and findings and to maintain focus on objectives.

Key review points included:

- An interim report presenting: a definition of a representative application of the FLM technique based on a proposed trial site installation; H&S Applicable Legislation review findings
- HAZOP workshop output
- Meeting with HSE
- Quantified Risk Assessment presentation to Electricity North West at a meeting on 22nd January 2018
- Electricity North West review of Safety Justification report

In addition, it is anticipated that an independent peer review will be conducted by another UK DNO having knowledge of and involvement in similar projects.

3 FAULT CURRENT LIMITING SERVICE

3.1 INTRODUCTION

Details of FCL service as it will be installed and operated when applied as part of business as usual are given in this section for the purposes of the safety justification. It was important to describe how FCL service will be realised and function in order that the potential hazards relating to the specific conditions could be established, evaluated and mitigated as required. This safety justification relates to the definition of FCL service given here.

It had been intended to trial the FCL methodology at a customer's site. However, no customers were willing to take part in such a trial and therefore the FCL service concept described in this report has not been trialled as yet and this report is based upon the generic scheme as described below.

A Fault Level Assessment Tool (FLAT) incorporated into Electricity North West's Network Management System has been developed as part of the Respond project. It assesses the network fault levels and has been considered as a method to control the enablement of the FLM techniques. However, it has been concluded based on the findings from the AP trial that the FLAT will not form part of the business as usual approach for the application of FCL service initially. Therefore, this definition of FCL service does not include FLAT functionality and it is taken to be permanently enabled for the purposes of this assessment. This safety assessment would need to be reviewed should enablement via the FLAT be subsequently incorporated into FCL service.

3.2 **DEFINITION**

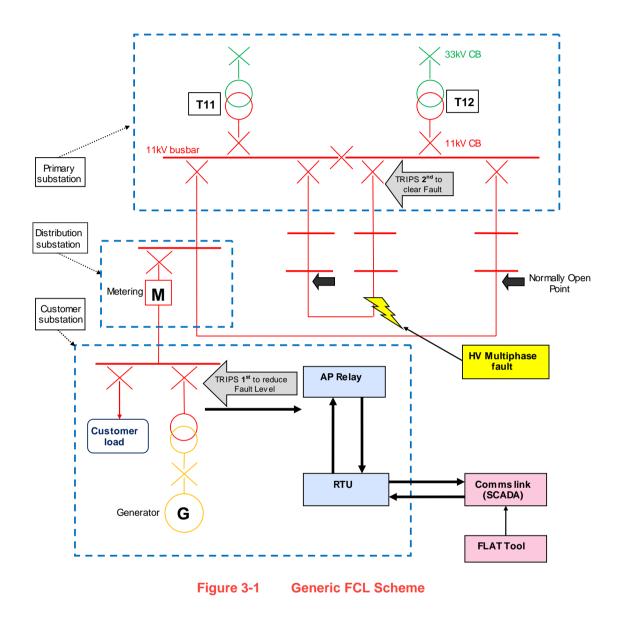
3.2.1 Installation

With FCL service, the network is reconfigured to reduce the fault current before the circuit breaker is opened to clear the fault as normal.

The generic design is shown in Figure 3.1 below and consists of an Argus-1 relay (the AP relay) and a tripping relay fitted to a panel situated within the customer's switch room. The AP relay has an input from the customer's existing switchgear CTs and is connected to the existing CB trip circuit via the tripping relay. There are also intputs to enable and disable the protection and outputs to monitor the protection status. The the Electricity North West's telecontrol (SCADA) system monitors the status and controls the AP relay via a remote terminal unit (RTU). The RTU has an internal battery powered from a standard 230V 13Amp socket; the relay panel requires a 110V DC supply from the existing substation battery or alternatively from a dedicated battery and charger.

Although the generic design incorporates the facility to control the FCL service through the FLAT tool it is assumed for the purposes of this safety case that the FCL service is permanently enabled and FLAT is not used. It is also assumed that:-

- a) There is only one customer load associated with any one primary substation
- b) The customer FCL installation would have a thorough proof test every 3 years



3.2.2 Operation

The current design of FCL service is only single stage and it is assumed that a second stage of operation would not be implemented because this would be unacceptable to customers as it would impose a greater service loss.

The FCL relay has a self-monitoring function which issues an alarm reflected in a warning in the network control room should the relay fail.

3.2.3 Network Conditions

FCL service will only be employed in networks when the following network conditions are met:

- i. The maximum prospective fault flow is within the peak make and break fault ratings of the bus section circuit breaker. (see safety requirement 25)
- ii. The maximum prospective fault flow is within the rating of the transformer and the peak make and break ratings of the transformer circuit breakers. (see safety requirement 18)
- iii. The maximum peak (asymmetrical) fault current flow that will be seen with FCL service protection installed and working is within the instantaneous fault withstand capability and thermal capability of the substation busbars and all circuit breakers, including the feeder circuit breakers, i.e. they can withstand the fault current until FCL service operates. (See Safety requirements 3, 4,11,12)
- iv. The maximum peak (asymmetrical) fault current flow that will be seen with FCL service protection installed and working is within the instantaneous fault withstand capability and thermal capability of the feeder cables and/or OHL, i.e. they can withstand the fault current until FCL service operates. (see safety requirements 8, 9, 24)
- v. It should be possible to reduce the fault current to within ratings by upstream switching in the event that circuit breaker control supplies are lost within the FCL fitted substation. (See Safety requirement 17)
- vi. The maximum prospective fault current even if FCL service fails is within the rating of existing customer switchgear on any feeder or the fault level at a customers' site is equal to or less than the design fault level (See Safety requirement 23)
- vii. FCL only to be applied where the prospective fault current is within the rating of existing distribution switchgear on any feeder even if FCL service fails to operate (See Safety requirement 22)

3.2.4 Maintenance

It is assumed that the FCL installation at the customer's site will be thoroughly tested every 3 years.

3.3 EXISTING USAGE

Previous and existing use of this FLM technique would be a useful source of information for producing a safety justification for this Electricity North West application. WSP therefore performed a thorough search regarding existing applications which concluded that this specific concept is unique.

In the UK two related techniques have been identified, presented below for completeness, but no information relevant to this present application could be determined:

• A similar approach of tripping generators for a different reason was identified and is presented below. As mentioned earlier, Electricity North West Fault Current Limiting

reduces fault current by reconfiguring the network so that less fault current flows from the upstream system in order to avoid exceeding the rating limits of protective equipment (circuit breakers). Although not exactly the same, National Grid's System to Generator Operational Intertrip balancing service³ is along the same lines. National Grid operates 'a Balancing Service of automatic tripping of the user's circuit breaker(s) resulting in the tripping of BM Unit(s) or (where relevant) Generating Unit(s) comprised in a BM Unit to prevent abnormal system conditions occurring, such as over-voltage, overload, system instability etc. after the tripping of other circuit breakers following power system fault(s)^{r4}. Circuits are prevented from exceeding their thermal limits under abnormal conditions, rather than fault conditions as is the case for AP.

• In addition, another concept that seems to be quite similar but from a different perspective is the System Integrity Protection Scheme (SIPS). This has been installed in the UK in 2008 and more specifically on the interconnection between Scottish Power and National Grid (Anglo-Scottish boundary). Within this framework, depending on predefined criteria, a trip command is selectively issued to Scottish Power generating units in less than 20ms in response to faults on the cross-boundary circuits.

According to the results of an internet based search, there are no identified international cases of the FCL service.

³ http://www2.nationalgrid.com/uk/services/balancing-services/system-security/intertrips/

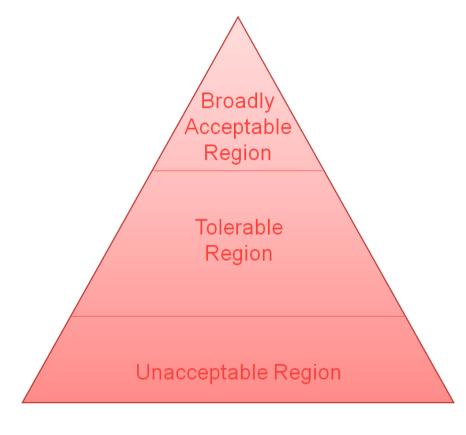
⁴ www2.nationalgrid.com/WorkArea/DownloadAsset.aspx?id=15308

4 TOLERABILITY OF RISK FRAMEWORK

The standard framework for tolerability of risk is explained in the HSE publication Reducing Risks Protecting People (R2P2)⁵.

R2P2 places risk into one of three regions: 'Unacceptable', 'Tolerable" and 'Broadly Acceptable'. These are depicted in Figure 4-1. As explained in Section 2.1 it is normally acceptable if risks in the tolerable region are reduced SFAIRP. However, in the case of FCL service, because it arguably contravenes Regulation 5, risks would need to be reduced to the "Broadly Acceptable" level.

Guidance in R2P2 has been used to determine the boundaries between the different regions.





The R2P2 guidance presents an upper tolerability limit for risk of death for an individual worker at 10⁻³ per annum and for an individual member of the public at 10⁻⁴ per annum.

The guidance also states that an individual risk of death at 10⁻⁶ per annum for both workers and the public corresponds to a very low level of risk and should be used as a guideline for the boundary between the 'Broadly Acceptable' and 'Tolerable' regions. The R2P2 tolerability limits for risk of death have been considered in the development of a risk framework for the Respond

⁵ http://www.hse.gov.uk/risk/theory/r2p2.pdf

project to assess the use of each of the three FLM techniques (Adaptive Protection, Is Limiter and Fault Current Limiting Service) on the Electricity North West electricity distribution network. A risk matrix for workers is presented in Table 4-1 and a risk matrix for the public is presented in Table 4-2 and these represent the summation of risk across Electricity North West from Respond schemes on a 'per hazard' basis. The individual risk is the probability for an exposed individual that they personally are killed or injured. Therefore, it is not the risk of a fatal accident but the risk to a specific individual being killed in that accident. For example, if there is one fatal accident that kills a substation worker per year and there are 50 substation workers the individual risk is 1 in 50 years.

The R2P2 boundary values correspond to all of the risks faced by workers and the public, whilst the use of FCL service is only one of these risks. Consequently, the HSE guidance has been calibrated for the specific hazards due to the use of FCL service and the resulting boundary conditions are shown in Figure 4-2 for a single substation site.

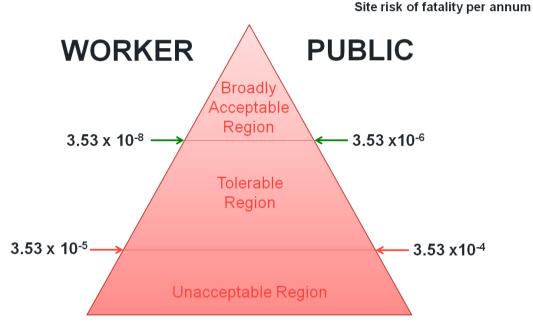


Figure 4-2 Specific Boundary values for RESPOND Project

These values can also be used as the basis for a matrix characterising the tolerability of risk presented by Respond hazards for workers (Table 4-1) and for the public (Table 4.2)

Risk Matrix (per hazard) - Workers

	FREQUENCY	FREQUENCY (per annum)				
SEVERITY	6 Frequent > 10 ⁻¹	5 Likely > 10 ⁻² <=10 ⁻¹	4 Occasional > $10^{-3} <= 10^{-2}$	$3 \text{ Infrequent} > 10^{-4} <= 10^{-3}$	2 Remote > 10 ⁻⁵ <=10 ⁻⁴	1 Highly improbable > 10 ⁻⁶ <=10 ⁻⁵
5 Serious	Unacceptable	Unacceptable	Unacceptable	Unacceptable	Tolerable	Tolerable
4 Significant	Unacceptable	Unacceptable	Unacceptable	Tolerable	Tolerable	Tolerable
3 Moderate	Unacceptable	Unacceptable	Tolerable	Tolerable	Broadly acceptable	Broadly acceptable
2 Minor	Unacceptable	Tolerable	Tolerable	Broadly acceptable	Broadly acceptable	Broadly acceptable
1 Negligible	Tolerable	Tolerable	Broadly acceptable	Broadly acceptable	Broadly acceptable	Broadly acceptable

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Table 4-1

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	FREQUENCY (per annum)					
SEVERITY	6 Frequent > 10 ⁻¹	5 Likely > 10 ⁻² <=10 ⁻¹	4 Occasional > $10^{-3} <= 10^{-2}$	3 Infrequent > $10^{-4} <= 10^{-3}$	2 Remote > 10 ⁻⁵ <=10 ⁻⁴	1 Highly improbable <=10 ⁻⁵
5 Serious	Unacceptable	Unacceptable	Unacceptable	Tolerable	Tolerable	Broadly acceptable
4 Significant	Unacceptable	Unacceptable	Tolerable	Tolerable	Broadly acceptable	Broadly acceptable
3 Moderate	Unacceptable	Tolerable	Tolerable	Broadly acceptable	Broadly acceptable	Broadly acceptable
2 Minor	Tolerable	Tolerable	Broadly acceptable	Broadly acceptable	Broadly acceptable	Broadly acceptable
1 Negligible	Tolerable	Broadly acceptable	Broadly acceptable	Broadly acceptable	Broadly acceptable	Broadly acceptable

Table 4-2 Risk Matrix (per hazard) – Public

FREQUENCY (per annum)

The consequence classifications (severity) used in the Respond risk matrices are defined in Table 4-3. They are based upon the safety descriptors from a risk appetite framework used by Electricity North West to qualitatively assess and manage risks in key areas of its business including safety.

Table 4-3 Consequence classifications

LEVEL	CONSEQUENCE	SAFETY/HEALTH DESCRIPTOR
1	Negligible	Slight injury not requiring treatment.
2	Minor	First aid / medical treatment is required.
3	Moderate	Time losing injury / health impact results.
4	Significant	A fatality / fatal occupational disease occurs or multiple Moderate injuries.
5	Serious	Multiple fatalities / fatal occupational diseases occur.

Each risk matrix has been calibrated for the Respond project to account for the expected hazards, at-risk population and contribution to the overall Electricity North West risk profile using the following equations for the upper limit of tolerable risk, with parameters defined in Table 4-4. For the purposes of this calibration it was judged reasonable that if Respond was widely adopted it may constitute up to 2% of an overall workers risk. It was also assessed that Respond would introduce approximately 10 hazards based on the initial hazard identification.

Worker fatality (per Respond hazard) per annum R_{WHT} = R_{IWT} x P_{WRE} x C_{PR} / H

Public fatality (per Respond hazard) per annum R_{PHT} = R_{IPT} x P_{PRE} x C_{PR} / H

PARAMETER	VALUE	DESCRIPTION
R _{IWT}	10 ⁻³ per annum	Upper limit of tolerability for risk of death of individual worker per annum.
P _{WRE}	500	Worker population exposed to Respond hazards, assuming Electricity North West/customer workforce of 2000 of which 25% operates in vicinity of switchgear.
C _{PR}	0.02	Contribution of Respond risk as proportion of overall Electricity North West risk (i.e. 2%).
н	10	Estimated number of hazards associated with Respond project fault level mitigation techniques.
R _{WHT}	10 ⁻³ per annum per hazard	Upper limit of tolerability for risk of death from single hazard associated with Respond project, calculated using equation $R_{IWT} \times P_{WRE} \times C_{PR} / H$
RIPT	10 ⁻⁴ per annum	Upper limit of tolerability for risk of death of individual member of the public per annum.
P _{PRE}	50,000	Public population exposed to Respond hazards, assuming

Table 4-4Risk matrix calibration

PARAMETER	VALUE	DESCRIPTION
		population density 0.0001 persons per m ² in risk zone.
R _{PHT}	10 ⁻² per annum per hazard	Upper limit of tolerability for risk of death from single hazard associated with Respond project, calculated using equation $R_{IPT} \times P_{PRE} \times C_{PR} / H$

Separately, the Energy Networks Association (ENA) has published guidance in its SHE Standard 07 Model Distribution Safety Rules (MDSR) which includes an approximation tool for risk assessment, refer to Figure 4-3. The derivation of the tool is not presented within the ENA standard, however a comparison has been undertaken between the tool and the risk tolerability matrices (Table 4-1 and Table 4-2) used in this document. There is a general correlation of results from both schemes although the risk matrices used in this document appear slightly more cautious than the ENA MDSR risk assessment scheme.

\backslash	/		Consequen	ces	
Probability Individuals of Exposure to Hazardous / Hazard	Individua Risk	I	VI	Multiple Fatalities	
Likely Event (% of time)	Level		v	Fatality	
1 in 10 - Frequent	Consequences		IV	Severe	Permanent disability / loss of sight
• /	(See Table)		ш	Major	Serious injury (effects reversible)
1 in 100 - Probable = <19	Multiple Fatalities - VI G	Unacceptable	ш	Minor	Injury requiring medical treatment
- 1%	Fatality V	Risk cannot be justified except in extraordinary circumstances	1	Insignificant	Bruising / First Aid injury
1 in 1000 — Occasional - 25%	Severe - IV		Exposure	(Based on working week of 5 X 8hr days)	
(10 ⁻³)	Severe A IV	Control measures must be introduced for risk in this region	to Hazard	per week	per day
- 50%	Major - III	to drive residual risk down towards the Low region.	0.5%	¾ hr	10 mins
- 75%	Major + VII E R	Λ	1%	1.5 hrs	20 mins
1 in 10,000 - Remote - 100% continuous		Tolerable only if cost of reduction	2.5%	3 ¼ hrs	45 mins
(104)		would exceed the improvement gained	5%	8 hrs	1 1/2 hrs
/ •	Insignificant-		7.5%	12 hrs	2 1/2 hrs
1 in 100 000 _ Improbable		Broadly acceptable Level of risidual risk regarded as	10%	16 hrs	3 hrs
1 in 100,000 — Improbable (10 ⁻⁵)	• 🔐 L	insignificant and further effort to reduce risks not likely to be required.	15%	24 hrs	5 hrs
/	w -	 Resources to reduce risks likely to 	20%	32 hrs	6.5 hrs
		be grossly disproportionate to the risk reduction achieved.	25%	40 hrs	8 hrs
1 in 1 million Remote			50%	80 hrs	16 hrs
(10 ⁴) TIE LI	NE		75%	120 hrs	24
/•			100%	160 hrs	24 hrs
/	V		1		

Figure 4-3 ENA risk assessment tool - extract from ENA SHE Standard 07 MDSR

5 LEGISLATIVE REVIEW

5.1 LEGISLATIVE FRAMEWORK

A review was conducted of H&S Applicable Laws and supplementary guidance relating to the implementation of a FCL service scheme in the UK. The review included:

- Health and Safety Work etc. Act 1974 (HSW Act)
- Management of Health and Safety at Work Regulations 1999
- Electricity at Work Regulations 1989 (EAW Regulations)
- EAW Regulations 1989 Guidance on Regulations HSR25 2015
- Electricity at Work: Safe Working Practices, HSG85, 2013
- Electricity Safety, Quality and Continuity Regulations 2002 (ESQC Regulations) with Amendments 2006 and 2009

Where significant requirements have been identified as applicable to changes introduced by FCL service to the DNO assets and operations, these have been included in Appendix D.

5.2 DISCUSSION OF REQUIREMENTS

For safety related applications, such as the FCL service scheme, the most relevant general legislation is the HSW Act which specifies that risks of injury associated with an undertaking shall be reduced 'So Far As Is Reasonably Practicable' (SFAIRP).

Similarly, the ESQC Regulations, particularly pertinent to the safety of design and implementation of an FCL service scheme, require that the associated risks of injury shall be reduced SFAIRP.

Requirements based on the SFAIRP principle are achievable by developing and implementing an FCL service scheme which is underpinned by a hazard identification and risk assessment process including demonstration that risks not 'Broadly Acceptable' are nevertheless 'Tolerable' and 'As Low As Reasonably Practical (ALARP)'.

The EAW Regulations, however, include three regulations conferring requirements upon an undertaking, such as the FCL service scheme, which are construed as absolute requirements:

- Regulation 5 "No electrical equipment shall be put into use where its strength and capability may be exceeded in such a way as may give rise to danger"⁶
- Regulation 11 "Efficient means, suitably located, shall be provided for protecting from excess of current every part of a system as may be necessary to prevent danger."
- Regulation 12 "Where necessary to prevent danger, suitable means (including, where appropriate, methods of identifying circuits) shall be available for: (a) cutting off the supply of electrical energy to any electrical equipment; and (b) the isolation of any electrical equipment."

⁶ In the EAW Regulations "danger" means risk of injury

HSR25, HSE guidance on the EAW Regulations, is particularly relevant to the implementation of the FCL service and provides clear interpretation of the meaning of the terms used in the regulations and of the purpose of each regulation.

HSR25 clause 58 states:

"If the requirement in a regulation is 'absolute', for example if the requirement is not qualified by the words 'so far as is reasonably practicable', the requirement must be met regardless of cost or any other consideration. Regulations making such absolute requirements are subject to the defence provision of regulation 29."

Appendix D cites several extracts from the HSR25 guidance associated with Regulations 5, 11 and 12 where the extracts explain the relevant requirements and how the 'absolute' and 'reasonably practicable' terms apply.

Regulations which contain 'absolute' requirements are therefore unequivocal.

FCL service is intended for use in cases where fault levels would potentially exceed equipment capability. If FCL service was to be applied in a case where the fault current could exceed the circuit breaker rating then, should the FCL service fail, it may be interpreted as being in contravention of EAW Regulations 5, 11 and 12.

HSE expressed the view, when consulted about this specific point, that failure of FCL service would contravene these regulations and that the defence against prosecution, in accordance with Regulation 29 of the EAW Regulations, would be that a person or organisation (i.e. Electricity North West) would need to prove that it had taken all reasonable steps and exercised due diligence to avoid commission of an offence against the Act. In the view of HSE this would be satisfied if any risks were shown to be "Broadly Acceptable" and hence the normal SFAIRP argument would not apply.

6 HAZARD IDENTIFICATION AND QUANTIFIED RISK ASSESSMENT

This section documents the hazards identified as associated with the FCL service scheme and presents the results of the risk assessment conducted to determine the level of risk presented by the scheme.

6.1 IDENTIFIED HAZARDS

The HAZOP exercise identified four hazards that represent a significant potential risk to workers on or close to the substations where FCL service is applied and to members of the public in close proximity to the affected substations or transmission cables. These are:

- e) Short circuit of the busbar in a substation resulting in excessive fault current
- f) Short circuit within a Circuit Breaker in the substation resulting in excessive fault current
- g) Short circuit of the feeder cables or something connected to these cables such that the feeder cable withstand current is exceeded
- h) Short circuit of the overhead line or something connected to the overhead line such that the overhead line withstand current is exceeded

For each of these hazards a quantified risk assessment has been conducted.

A further 19 hazards were identified which presented no significant change to the situation existing without FCL service applied. The complete list of hazards is included at Appendix A.

6.2 QRA METHODOLOGY

Event Tree has been used as the QRA methodology. This starts with the initiating event (e.g. feeder cable short circuit) and then considers how this can develop into a range of possible outcomes including fatality and other accident scenarios. In general, the event tree for each hazard progresses with the FCL service failure resulting in an explosion and then with either a worker or a member of the public in critical proximity they are killed by the explosion.

By considering the frequency of the initiating event and the probabilities of each of the subsequent steps in the accident chain the overall frequency of accidents is calculated.

6.3 INPUT DATA

6.3.1 Frequency of Initiating Events

The frequency of each of the initiating events has been estimated using available data as summarised in Table 6.1.

PARAMETER	VALUE	SOURCE			
Short circuit within a circuit breaker	0.0022 per FCL site per annum	Based on a failure rate for all circuit breaker faults from NAFIRS ⁷ , adjusted using values from the IEEE Gold Book for the proportion of failures that are short circuits and allowing for 10 circuit breakers on average per site.			
Short circuit of the feeder cables	0.322 per FCL site per annum	Based on a failure rate from NAFIRS data for Electricity North West per 100km of cable and assuming (based on fault current estimates) that an excessive fault current could only arise due to a short circuit in the first 700m of cable and that on average there are 10 feeder cables per substation. It is assumed that all short circuits will develop from phase to earth to phase to phase before feeder CB operates.			
Short circuit of the overhead line	0.4284 per FCL site per annum	Based on a failure rate from NAFIRS data for Electricity North West per 100km of overhead line and assuming (based on fault current estimates) that an excessive fault current could only arise due to a short circuit in the first 700m of overhead line and that on average there are 6 feeders per substation. It is assumed that all short circuits will develop from phase to earth to phase to phase before feeder CB operates.			

Table 6-1 Frequency of initiating events

6.3.2 Probability of FCL service Failure

The FCL service function will fail if either the FCL service relay or the associated circuit breaker fails. The calculation takes account of the percentage of failures that are detected by the relay self-diagnostic function and are flagged up to the operator for rectification (assumed within 8 hours) and those that are not detected.

Table 6-2 FCL failure input data

PARAMETER	VALUE	SOURCE
Relay Total failure Rate	0.042 per Relay per annum	Manufacturers data
Relay Undetected Failure Rate	0.0042 per Relay per annum	Conservative estimate that 90% of failures will be either detected by diagnostics or will cause a trip when it should not
Circuit Breaker Total failure rate	0.0022 per relay per annum	Based on failure rate from NAFIRS data for Electricity North West
Circuit breaker failure to operate on demand	0.00022 per relay per annum	From Gold Book failure mode data that 10% of failures are found on test or are failure to open

Using the above figures, a probability that FCL service fails to operate on demand has been calculated as 0.0067. This falls within the SIL 2 level of BS EN61508 (between 1 in 100 and 1 in 1000 probability of failure on demand). Hence a production FCL service system would need to be developed to meet SIL 2 requirements.

⁷ National Fault and Interruption Reporting Scheme

6.3.3 Probability of Worker Fatality

The probability of a worker fatality in the event of an explosion due to an initiating event has been estimated as 0.00001. This assumes that there is a procedure in place such that the network will be reconfigured to reduce fault level within equipment capabilities before a worker enters the substation. Given that these sites are unmanned the normal probability that a worker is in a substation has been estimated at 90 hours per year (i.e. 1% of the time) by the HAZID workshop team. Given the procedure of reconfiguration before a worker enters a site, it is expected the probability of this procedure failing is 1 in 100. The probability that the worker is actually killed by the explosion resulting from FCL service failing has been estimated as 0.1. Together these assumptions lead to the overall probability of a worker being killed of 0.01*0.01*0.1 = 0.00001.

6.3.4 Probability of Public Fatality

The probability of a member of the public being killed in the event of an explosion event is dependent on the specifics of the site. For the purposes of this analysis it has been assumed there are high, medium and low risk sites.

A high risk site has been defined as a site where the risk of public fatality is high (between 0.3 and 0.03 or 1 in 3 to 1 in 30). This means that people would need to be present a high percentage of the time and also that an explosion due to the release of the fault energy would need to present a risk to these people either because the substation itself collapses and the people are close enough to be killed by the collapse or because of a feeder cable failing due to excess fault current is directly underneath a person and the ground or cable duct does not contain the release of the energy. The Event Tree analysis has assumed the geometric mean case (0.1) for high risk substations.

A medium risk site has been defined as a site where the risk of public fatality is medium (between 0.03 and 0.003 or 1 in 30 to 1 in 300). This means that people would need to be present for a significant percentage of the time and also that any explosion would need to present a risk to these people either because the substation itself collapses and the people are close enough to be killed by the collapse or because the feeder cable failing due to excess fault current is directly underneath a person and the ground or cable duct does not contain the release of energy. The Event Tree analysis has assumed the geometric mean case (0.01) for medium risk substations.

A low risk site has been defined where the risk of public fatality is low (less than 0.003 or 1 in 300). The Event tree analysis has assumed a value of 0.001 for low risk substations (geometric mean of 0003 to 0.0003).

An example of a high risk site would be where there is a substation in a busy area (e.g. a shopping centre) and that site was not protected against explosions inside the substation or of the cable and the cable is not rated for the fault current that could occur if FCL failed. In reality it is suspected that sites in this type of situation are likely to incorporate measures to protect against explosions because there are already possible causes of such explosions on these sites but this has to be allowed as a possibility.

An example of a medium risk site would be an urban site where the feeder cable runs under the pavement at a school entrance and could rupture due to excess fault current and the failure is not contained. If it is estimated that people gather outside school gates around 2 hours per day (1 in 10) and that these people occupy 35m out of the possible 700m failure zone for the feeder cable (1 in 20). This gives an overall risk of 1 in 200 which is within the medium risk boundaries.

Another example of a medium risk site would be an urban site where a house is situated in the substation building collapse zone and substation is not blast proof. It is estimated that the risk that the building collapses on the side where the house is situated is 1 in 4 and the risk that the building is occupied at the time is 1 in 2 and then that the person(s) in the house are killed is 1 in 5. This gives a total risk of 1 in 40 which is medium risk.

6.4 QRA RESULTS

The Event Trees are presented in Appendix A and summarised in the Table below which compares the overall risk with the targets for 'Tolerable' and also 'Broadly Acceptable'. They are also shown graphically in Figure 6-1. It should be noted that the low risk category includes feeder cable substations and also those with overhead line feeders. These have slightly different risks. It has been assumed that no medium or high risk sites have overhead line feeders because these are generally only used in rural situations.

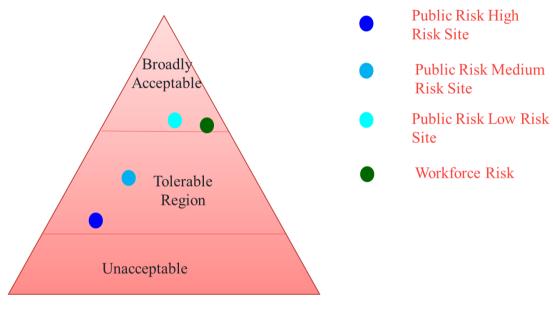


Figure 6-1 Respond FCL Risks

Table 6-3	QRA Results	5				
Consequence	Frequency per site per annum	'Tolerable' upper limit per site per annum (all Respond hazards)	Meets 'Tolerable' upper limit?	'Broadly Acceptable' limit per site per annum	Meets 'Broadly Acceptable' limit?	Further risk reduction factor required for 'Broadly Acceptable'
Public fatality High Risk	2.25E-04	3.54E-04	Yes	3.54E-06	No	63.4
Public fatality Medium Risk	2.25E-05	3.54E-04	Yes	3.54E-06	No	6.3
Public fatality Low Risk (Overhead Line)	2.96E-06	3.54E-04	Yes	3.54E-06	Yes	
Public fatality Low Risk (Feeder Cable)	2.25E-06	3.54E-04	Yes	3.54E-06	Yes	
Workforce Fatality	2.60E-08	3.53E-05	Yes	3.53E-08	Yes	

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6.5 DISCUSSION OF RESULTS

The QRA results indicate on the basis of the adopted methodology and all assumptions, that the requirement that risks should be reduced to the "Broadly Acceptable" level as advised by HSE is met for the low risk sites but not for medium or high risk sites.

6.6 SENSITIVITY ANALYSIS

The analysis in this report is based upon a number of estimates and assumptions which might be subject to challenge and review. Overall it is believed that the results are realistic or likely conservative because the failure rates are based on actual failure data, either for Electricity North West or, in the case of the relays, from a relay manufacturer. It is estimated that the probability of a worker entering an FCL service site without it being reconfigured beforehand so as to reduce fault currents (which is part of the agreed procedures) is 1 in 100. Given that the worker would clearly be putting themselves at risk and that the industry understands the importance of correct operation to protect people it is felt that this is a reasonably conservative assumption. It is assumed that if there is a network fault then a circuit breaker or cable carrying fault current above its rating will fail in an explosive manner whilst in reality it is quite possible that it may actually withstand the increased current. It is also assumed that all faults in feeder cables or OHL would develop from phase to earth to phase to phase before the feeder CB operates, which is a clearly conservative assumption.

Thus, the conclusions are regarded as reasonably robust.

6.7 SAFETY REQUIREMENTS

The risk assessment has identified safeguards, controls and mitigation measures necessary to manage the level of risk associated with the implementation of the defined FCL service scheme. These become the safety requirements which the FCL service implementation must achieve to ensure control of the risk associated with each of the hazard scenarios and for the defined FCL service scheme to present a 'Tolerable' level of safety risk. Referring to the complete list of safety requirements presented in Appendix C, these include:

a) Application conditions that must be satisfied before applying FCL service to a site, i.e. pre-requisites

SRs 3, 4, 8. 9, 11, 12, 17, 18, 22, 23, 24, 25

b) Safety function and performance measures necessary for the FCL system, including safety integrity level

SRs 1, 2, 6, 13, 15, 20, 21

c) Risk reduction measures for high risk sites to reduce risk to medium risk.

SR 7

 Implementation, operating and maintenance measures necessary to control safety risk of the FCL service scheme in use, including compliance with safety management systems, standards, procedures and codes of practice.

SRs 5, 10, 14, 16, 19, 20

It should be noted that the requirement that feeder circuit breakers and busbars can both withstand the fault currents up until the point where FCL service protection has operated is particularly difficult to demonstrate compliance with. In particular, the specification for existing circuit breakers gives a 3 second through current rating that is the same as the maximum break current and therefore if the maximum break current is exceeded (which is the reason why FCL service would be employed in the first case) then this 3 second current rating would be exceeded. The time for FCL service to operate is estimated to be 400ms and therefore in order to comply with the safety requirement the circuit breaker would need to be able to withstand the worst case fault current for up to 400ms. Whilst the 3 second fault current is based on thermal considerations and therefore a higher current could be withstood for 400ms there is no hard evidence that this would apply to the mechanical withstand capability, and such evidence would need to be established as part of the FCL service project. A similar argument would apply to the busbars.

6.8 NEXT STEPS

Tasks required to finalise this safety justification include:

- Electricity North West requests an independent DNO to conduct a formal review of this safety justification in order to increase stakeholder participation and strengthen the value of the report. Another DNO (UK Power Networks) has already been briefed on the approach, methodology and findings of this FCL service safety justification and so may be a useful party to seek this further engagement from.
- Electricity North West conduct a formal review of this safety justification to confirm that objectives have been achieved and to use as input to develop a plan for possible future implementation of an FCL service scheme.

The potential for a wider future development and implementation of an FCL service scheme is included in Section 7.2.

7 CONCLUSIONS

7.1 SUMMARY

This study has proposed a safety justification for implementation of the defined FCL service scheme within the Electricity North West network.

The analysis has shown that, based on arguably conservative assumptions, it would be acceptable from a safety viewpoint to fit low risk substations with an FCL service system but not high or medium risk sites. The FCL service system would be required to meet the SIL2 requirements of BS EN 61508.

Using recognised safety assessment processes, hazards associated with the FCL service scheme have been identified. Means of eliminating, controlling or mitigating the potential consequences of these hazards have been established. A quantified risk assessment has been performed which demonstrates the residual safety risk presented to workers and to members of the public by the defined scheme.

Four hazard scenarios associated with the implementation of the defined FCL service scheme have been determined to present the most significant risk. These include the potential for the failure of feeder cables and fire and/or structural damage at substations, possibly causing injuries and fatality for workers and members of the public.

Safety requirements (further to those already in place for the existing network and operations) have been established by the risk assessment based on the detailed input data and assumptions. Achievement of these safety requirements would ensure control of the risk associated with each of these scenarios and the defined FCL service scheme would present a Tolerable safety risk. The safety requirements include:

- a) Application conditions that must be satisfied before applying FCL service to a site, i.e. pre-requisites
- b) Safety function and performance measures necessary for the FCL system, including safety integrity level
- c) Implementation, operating and maintenance measures necessary to control safety risk of the FCL service scheme in use, including compliance with safety management systems, standards, procedures and codes of practice.

The study has also reviewed the requirements laid down by health and safety applicable legislation relevant to the defined FCL service scheme. This identified 'absolute' requirements of the EAW Regulations, specifically Regulations 5, 11 and 12 which, unlike other legislation requirements, are not satisfied by 'reasonably practicable' risk control measures and safety arguments. The EAW Regulations, Regulation 29, sets out the means for a legal defence in the event these 'absolute' regulations are breached.

This point has been discussed with HSE and a point of view offered by HSE was that provided a risk assessment had been performed which justified that the risk presented by the FCL service scheme was 'Broadly Acceptable' then this would support an Electricity North West claim that it had taken sufficient steps to comply with the Regulations.

The study has therefore considered steps that could be taken by Electricity North West to demonstrate that risks associated with the defined FCL service scheme are 'Broadly Acceptable' for all scenarios.

The study considered the robustness of the input data and assumptions and determined that some current data and assumptions could be over-pessimistic. Where a justification could be made to refine these then that may remove the need for the additional measures for substation structures and cable duct protection at high risk sites.

7.2 FURTHER DEVELOPMENT TO SUPPORT FUTURE IMPLEMENTATION

It is proposed that Electricity North West requests an independent DNO such as UK Power Networks to conduct a formal review of this safety justification in order to increase stakeholder participation and strengthen the value of the report. UK Power Networks has already been briefed on the approach, methodology and findings of this FCL service safety justification and so may be a useful party to seek this further engagement from.

It is recommended that Electricity North West conducts a formal review of this safety justification to confirm that objectives have been achieved and to use as input to developing a plan for possible future implementation of an FCL service scheme and incremental safety justifications. The results of this will inform future steps in the development and application of the technique.

The scope of this study has been purposely constrained to consideration of safety associated with implementing the defined FCL service scheme. It is recommended that additional investigation and analysis of a possible FCL service scheme is performed by Electricity North West in areas such as business and operational risk, cost, legal implications and business strategy to contribute to the business case.

Subject to these additional steps, it is recommended that Electricity North West takes forward the development of the FCL service scheme with appropriate level of validation of achievement of the required SIL for the solutions adopted. As part of this it would be specifically required to establish that the short term (approx. 400ms) current withstand of circuit breakers and busbars is higher than current published 3 second ratings.

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APPENDIX A HAZARD LIST

ID	HAZARD	CONSEQUENCE
1	Transformer high current caused by short circuit fault in the downstream system, i.e. on a feeder circuit.	Inconsequential. Transformers are rated on x 3 fault current.
2	Increased fault current flowing through the transformer causes increased oil degradation.	Inconsequential. Operation within rating and for a short time, causing insignificant change to the existing (non- FCL) situation with regards oil degradation and ageing.
3	Transformer CB high current caused by short circuit fault in the downstream system, i.e. on a feeder circuit.	Inconsequential. Higher fault level currents than usual but within rating. Operation within rating causing insignificant change to the existing situation.
4	Increased fault current flowing through the transformer CB may cause additional degradation.	Inconsequential. Operation within rating causing insignificant change to the existing situation.
5	Bus coupler high current caused by short circuit fault in the downstream system, i.e. on a feeder circuit.	Inconsequential. Operation within rating causing insignificant change to the existing situation.
6	Increased fault current flowing through the bus coupler CB may cause additional degradation.	Inconsequential. Operation within rating causing insignificant change to the existing situation.
7	Busbar A/B high current caused by short circuit fault at the busbar.	The busbar will see a peak current and thermal impact. The peak asymmetrical fault current may be in excess of the busbar through fault current withstand rating. Excessive thermal conditions or excessive forces leading to explosion (substation structural damage) and potential fatality (workers and public).
8	Short circuit causing fault level currents in substation equipment in excess of ratings.	Explosion that could cause damage to structures and consequential potential fatality (workers and public).
9	Feeder cables high current caused by short circuit fault.	Increased fault level current could cause cable thermal rating to be exceeded (l^2t) , excessive current, cable damage, cable joint explosion, substation structural damage and potential fatality (workers and public). Potentially involving interruption of adjacent utilities.
10	Feeder CB high current caused by short circuit fault at the CB.	CB required to operate beyond its rating and may not be able to interrupt the fault current. Excessive thermal conditions or excessive forces could lead to fire and explosion with potential fatality (workers and public).
11	Failure of CTs connected to the feeder CB relay.	Feeder CB will not trip when a fault current occurs, CB through fault rating may be exceeded, could lead to fire and explosion with potential fatality (workers and public).
12	Feeder CB oil degradation and increased contact wear caused by operation at higher fault levels.	Degraded operation is more likely, as is failure on demand.
13	Feeder CB oil degradation and increased contact wear caused by insufficient maintenance.	Degraded operation is more likely, as is failure on demand.
14	FCL protection fault caused by loss of supply voltage or loss of CTs input (relay monitoring).	Public and workers potentially exposed to hazards due to fire or explosion resulting from any separate fault current conditions occurring between FCL protection failure and control engineer action to mitigate it.

 ID	HAZARD	CONSEQUENCE
15	FCL relay protection loss of communication to detect FCL relay health.	Public and workers potentially exposed to hazards due to fire or explosion resulting from any separate fault current conditions occurring between FCL protection loss and control engineer action to mitigate it in response to 'loss of FCL health' warning.
16	FCL relay protection failure due to loss of supply on substation / no battery backup.	Public and workers potentially exposed to hazards due to fire or explosion resulting from any separate fault current conditions occurring between FCL protection loss and control engineer action to mitigate it in response to 'loss of FCL health' warning.
17	Breaker failure of FCL CB	No response to open command. No fault level reduction when required. Public and workers potentially exposed to hazards due to fire or explosion resulting from any separate fault current conditions occurring.
18	FCL not operational when required due to incorrect or inappropriate FCL relay settings.	Reduced or zero level of FCL. Public and workers potentially exposed to hazards due to fire or explosion resulting from any separate fault current conditions occurring.
20	FCL not operational when required due to faulty or damaged CTs.	Reduced or zero level of FCL. Public and workers potentially exposed to hazards due to fire or explosion resulting from any separate fault current conditions occurring.
21	Customer switchgear high current due to short circuit fault.	Switchgear required to operate with excessive current and/or excessive thermal conditions, could lead to fire and explosion with potential fatality (workers and public).
22	Distribution switchgear high current due to short circuit fault.	Switchgear required to operate with excessive current and/or excessive thermal conditions, could lead to fire and explosion with potential fatality (workers and public).
23	Overhead lines (OHL) high current due to short circuit fault.	Could cause cable thermal rating to be exceed $(I^{2}t)$ Increased fault level current could cause cable thermal rating to be exceeded $(I^{2}t)$, excessive current, cable damage, cable clearance limits being exceeded, substation structural damage and potential fatality (workers and public).

APPENDIX B EVENT TREES

Short circuit of the busbar in a substation resulting in excessive fault current

Busbar A/B high current due to short circuit fault.	FCL Service operation	Personnel comply with exclusion procedure for	Public not in fatality risk zone at time of hazard	All consequences (per site)	Frequency (per annum across ENW)
short circuit fault.					(per annum across EN W)
		operating substation. Personnel not in fatality	occurrence. (Figure is for High Risk)		
		risk zone at time of	High Risk)		
		hazard occurrence.			
2.15			N 1	4 425 22	
λ (frequency per annum per	N (detected fault)	Ν	Ν	1.42E-02	
site)			_		
0.01423669	0.000367253	0.00001	0		
			Y		
			1	Workforce fatality.	1.48E-08
				Severe asset damage.	
		Y	Ν		
		0.99999	0.1	Public fatality.	1.48E-04
				Severe asset damage.	
			A		
			0.9	Severe asset damage.	1.33E-03
	N (undetected fault)	N	N		
	0.006306306	0.00001	0		
			Y		
			1	Workforce fatality	2.54E-07
				Severe asset damage.	
		Y	Ν		
		0.99999	0.1	Public fatality.	2.54E-03
				Severe asset damage.	
			Y		
			0.9	Severe asset damage.	2.29E-02
	Y				
	0.993326441			Asset fault.	4.00E+00
	0.555520771			Service limitation.	1.002.00
				Maintenance activity.	
				mannenance activity.	

Short circuit of the feeder cables or something connected to these cables such that the feeder cable withstand current is exceeded

Feeder cables high current with	FCL Service operation	Personnel comply with	Public not in fatality risk	All consequences (per site)	Frequency
cable thermal rating		exclusion procedure for	zone at time of hazard		(per annum across ENW)
exceedance (I^2t) due to short		operating substation.	occurrence.		
circuit fault.		Personnel not in fatality			
		risk zone at time of			
		hazard occurrence.			
λ (frequency per annum per	N (detected fault)	Ν	Ν	3.22E-01	
site)					
0.322	0.000367253	0.00001	0		
			Υ		
			1	Workforce fatality.	3.35E-07
				Severe asset damage.	
		Y	N		
		0.99999	0.1	Public fatality.	3.35E-03
				Severe asset damage.	
			Y		
			0.9	Severe asset damage.	3.01E-02
	N (undetected fault)	Ν	N		
	0.006306306	0.00001	0		
			Y		
			1	Workforce fatality.	5.75E-06
				Severe asset damage.	
		Y	Ν		
		0.99999	0.1	Public fatality.	5.75E-02
				Severe asset damage.	
			Y		
			0.9	Severe asset damage.	5.17E-01
	Y				
	0.993326441			Asset fault.	9.05E+01
				Service limitation.	
				Maintenance activity.	

Feeder CBs high current due to	FCL Service operation	Personnel comply with	Public not in fatality risk	All consequences (per site)	Frequency
short circuit fault.		exclusion procedure for operating substation. Personnel not in fatality risk zone at time of hazard occurrence.	zone at time of hazard occurrence.		(per annum across ENW)
λ (frequency per annum per site)	N (detected fault)	Ν	N	2.20E-04	
0.00022	0.000367253	0.00001	0		
			Y		
			1	Workforce fatality.	2.29E-10
				Severe asset damage.	
		Y	Ν		
		0.99999	0.1	Public fatality.	2.29E-06
				Severe asset damage.	
			Y		
			0.9	Severe asset damage.	2.06E-05
	N (undetected fault)	Ν	N		
	0.006306306	0.00001	0		
			Y		
			1	Workforce fatality.	3.93E-09
				Severe asset damage.	
		N .	N		
		γ	N		0.005.05
		0.99999	0.1	Public fatality.	3.93E-05
				Severe asset damage.	
			N .		
			Y 0.9	Covere asset damage	3.53E-04
			0.9	Severe asset damage.	3.33E-U4
	v				
	<u>ү</u> 0.993326441			Asset fault.	6.18E-02
	0.993320441			Service limitation.	0.10E-02
				Maintenance activity.	
	1	1	1		1

Short circuit within a Circuit Breaker in the substation resulting in excessive fault current

Short circuit of the Overhead Line or something connected to the Overhead Line such that the Overhead Line withstand current is exceeded

Overhead lines (OHL) high	FCL Service operation	Personnel comply with		All consequences (per site)	Frequency
current with cable thermal		exclusion procedure for	zone at time of hazard		(per annum across ENW)
rating exceedance (I^2t) due to		operating substation.	occurrence.		
short circuit fault.		Personnel not in fatality			
		risk zone at time of			
		hazard occurrence.			
λ (frequency per annum per	N (detected fault)	N	Ν	4.28E-01	
site)	(************************				
0.4284	0.000367253	0.00001	0		
			Y		
			1	Workforce fatality.	4.45E-07
				Severe asset damage.	
		Y	Ν		
		0.99999	0.1	Public fatality.	4.45E-03
				Severe asset damage.	
			Y		
			0.9	Severe asset damage.	4.01E-02
	N (undetected fault)	Ν	Ν		
	0.006306306	0.00001	0		
			Y		
			1	Workforce fatality.	7.65E-06
				Severe asset damage.	
		Y	Ν		
		0.99999	0.1	Public fatality.	7.65E-02
				Severe asset damage.	
			Y		
			0.9	Severe asset damage.	6.88E-01
	Υ				
	0.993326441			Asset fault.	1.20E+02
				Service limitation.	
				Maintenance activity.	

APPENDIX C SAFETY REQUIREMENTS

ID.	RELATED HAZARDS	DESCRIPTION
SR1	7, 8,9,10,11,	Apply FCL
	23	
SR2	7, 9, 10, 11, 23	Overcurrent protection - Tx HV side (where required)
SR3	7, 9, 10, 11, 23	Busbar able to withstand peak instantaneous fault current if FCL is installed and working
SR4	7, 9, 10, 11, 23	Busbar able to withstand the worst case thermal (I^2t) impact if FCL is installed and working
SR5	7, 9, 10, 11, 23	Before workforce enter substation, ensure operational procedures are followed to reduce prospective fault current to within
		limits (open busbar CB)
SR6	7, 9, 10, 11, 23	FCL target failure measure Safety Integrity Level (SIL) 2 as determined by risk assessment
SR7	7, 8, 9, 10, 11, 23	Substation structure explosion withstand capability; blast wall, additional containment, pressure relief (For high risk sites)
SR8	9	Feeder cables able to withstand maximum fault current if FCL is installed and working
SR9	9	Feeder cables able to withstand the thermal impact due to the flow of the worst case fault current if FCL is installed and
		working
SR10	12, 13	Maintenance of CBs, Txs and busbars should appropriately reflect the frequency of operation
SR11	9, 10, 11, 23	Feeder CB able to withstand the peak making current if FCL is installed and working
SR12	9, 10, 11, 23	Feeder CB able to withstand the prospective thermal (I^2t) impact if FCL is installed and working
SR13	14, 15, 19	FCL only to be applied where there is an alarm/warning system in the Control Room to indicate an FCL relay issue/problem
SR14	14, 15, 19	Control engineer manually issues a signal to open the bus section to mitigate the fault level issue, in response to FCL relay alarm
SR15	5 16	Alarm/warning system in the Control Room to indicate substation power supply fault/loss.
SR16	5 16	Control engineer manually issues a signal to operate upstream protection, in response to 'substation power supply fault/loss'
		alarm

ID.	RELATED HAZARDS	DESCRIPTION
SR17	16	FCL should only be applied where the fault level can be brought within rating by switching upstream.
SR18	1,2,3,4	Transformer fault currents are within the rating of the transformer and its circuit breaker even if FCL protection fails
SR19	17	Periodic proof testing of FCL system to confirm that all components are functioning as intended and free of faults
SR20	18	Planning to specify appropriate settings for FCL which are revised when any connections are added to the network to ensure that the switchgear is adequately rated, revised when the fault level changes, revised if the network is reconfigured or altered in a way that would change the prospective fault current at any location within the network
SR21	18	Satisfactory commissioning of FCL protection relays
SR22	21	FCL only to be applied where the prospective fault current is within the rating of existing customer switchgear on any feeder or the fault level at a customers' site is equal to or less than the design fault level even if FCL fails to operate
SR23	22	FCL only to be applied where the prospective fault current is within the rating of existing distribution switchgear on any feeder even if FCL fails to operate
SR24	23	FCL only to be applied where the worst case anticipated fault current is within the thermal capacity of any overhead lines for 400ms.
SR25	5,6	Bus coupler fault currents are within the rating of its circuit breaker even if FCL protection fails

APPENDIX D KEY REQUIREMENTS OF HEALTH & SAFETY APPLICABLE LEGISLATION

Note: The table below is not a complete definition of requirements from legislation applying to the design, implementation of an FCL scheme. It presents extracts from some relevant legislation and supplemental guidance – refer to original Acts, Regulations and associated supplemental guidance publications for a full description of requirements.

LEGISLATION REFERENCE DESCRIPTION

AND GUIDANC	Ε
HSW Act	Part 1, General duties of employers to their employees: It shall be the duty of every employer to ensure, so far as is reasonably practicable, Section 2 (1) the health, safety and welfare at work of all his employees.
	Part 1, General duties of employers to their employees:
	Section 2 (2) (a) the provision and maintenance of plant and systems of work that are, so far as is reasonably practicable, safe and without risks to health;
	(b) arrangements for ensuring, so far as is reasonably practicable, safety and absence of risks to health in connection with the use, handling, storage and transport of articles and substances;
	(c) the provision of such information, instruction, training and supervision as is necessary to ensure, so far as is reasonably practicable, the health and safety at work of his employees;
	(d) so far as is reasonably practicable as regards any place of work under the employer's control, the maintenance of it in a condition that is safe and without risks to health and the provision and maintenance of means of access to and egress from it that are safe and without such risks;
	(e) the provision and maintenance of a working environment for his employees that is, so far as is reasonably practicable, safe, without risks to health, and adequate as regards facilities and arrangements for their welfare at work.
	Part 1, General duties of employers and self-employed to persons other than their employees: It shall be the duty of every employer to Section 3 (1) conduct his undertaking in such a way as to ensure, so far as is reasonably practicable, that persons not in his employment who may be affected thereby are not thereby exposed to risks to their health or safety.
	Part 1, General duties of manufacturers etc. as regards articles and substances for use at work. It shall be the duty of any person who Section 6 (1) designs, manufactures, imports or supplies any article for use at work-
	(a) to ensure, so far as is reasonably practicable, that the article is so designed and constructed that it will be safe and without risks to health at all times when it is being set, used, cleaned or maintained by a person at work;
	(b) to carry out or arrange for the carrying out of such testing and examination as may be necessary for the performance of the duty imposed on him by the preceding paragraph.

Part 1, It shall be the duty of any person who undertakes the design or manufacture of any article for use at work to carry out or arrange for Section 6 (2) the carrying out of any necessary research with a view to the discovery and, so far as is reasonably practicable, the elimination or minimisation of any risks to health or safety to which the design or article may give rise. Management of HSW Regulations Regulation 3, Risk assessment: Every employer shall make a suitable and sufficient assessment of: (1) a) The risks to the health and safety of persons not in his employment arising out of or in connection with the conduct by him of his undertaking. EAW Regulations Regulation 4, All systems shall at all times be of such construction as to prevent, so far as is reasonably practicable, danger. (1) Regulation 5 No electrical equipment shall be put into use where its strength and capability may be exceeded in such a way as may give rise to danger. (1) Regulation 5 No electrical equipment which may reasonably foreseeably be exposed to: (a) mechanical damage; (b) the effects of the weather, natural hazards, temperature or pressure; (c) the effects of we, dirity, dusty or corrosive conditions; or (d) any flammable or explosive substance, including dusts, vapours or gases, shall be of such construction or as necessary protected as to prevent, so far as is reasonably practicable, danger arising from such exposure. Regulation Efficient means, suitably located, shall be provided for protecting from excess of current every part of a system as may be necessar 11 to prevent danger. Regulation Where necessar
HSW Regulations (1) a) The risks to the health and safety of his employees to which they are exposed whilst they are at work; and b) The risks to the health and safety of persons not in his employment arising out of or in connection with the conduct by him of his undertaking. EAW Regulations Regulation 4, All systems shall at all times be of such construction as to prevent, so far as is reasonably practicable, danger. (1) Regulation 5 No electrical equipment shall be put into use where its strength and capability may be exceeded in such a way as may give rise to danger. (1) Regulation 6 Electrical equipment which may reasonably foreseeably be exposed to: (a) mechanical damage; (b) the effects of the weather, natural hazards, temperature or pressure; (c) the effects of wet, dirty, dusty or corrosive conditions; or (d) any flammable or explosive substance, including dusts, vapours or gases, shall be of such construction or as necessary protected as to prevent, so far as is reasonably practicable, danger arising from such exposure. Regulation Efficient means, suitably located, shall be provided for protecting from excess of current every part of a system as may be necessar 11 to prevent danger. Regulation Where necessary to prevent danger, suitable means (including, where appropriate, methods of identifying circuits) shall be available 12, (1) for: (a) cutting off the supply of electrical energy to any electrical equipment; and
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12, (1) for-:(a) cutting off the supply of electrical energy to any electrical equipment; and
Regulation In any proceedings for an offence consisting of a contravention of regulations 4(4), 5, 8, 9, 10, 11, 12, 13, 14, 15, 16 or 25, it shall 29 be a defence for any person to prove that he took all reasonable steps and exercised all due diligence to avoid the commission of that offence.
HSR25 2015 Absolute/ Reasonably Practicable
Clause 57 Duties in some of the Regulations are subject to the qualifying term 'reasonably practicable'. Where qualifying terms are absent the requirement in the regulation is said to be absolute. The meaning of reasonably practicable has been well established in law. The interpretations in paragraphs 59–60 are given only as a guide to dutyholders.
Clause 58 If the requirement in a regulation is 'absolute', for example if the requirement is not qualified by the words 'so far as is reasonably practicable', the requirement must be met regardless of cost or any other consideration. Regulations making such absolute requirements are subject to the defence provision of regulation 29.
Regulation 5
Clause 80 The defence (regulation 29) is available in any proceedings for an offence under this regulation.

AND GUIDANCE	
	Before equipment is energised, the characteristics of the system to which the equipment is connected must be taken into account. This should include those existing under normal conditions, possible transient conditions and prospective fault conditions, so that the equipment is not subjected to stress which it is not capable of handling without giving rise to danger. The effects to be considered include voltage stress and the heating and electromagnetic effects of current.
	The term 'strength and capability' of electrical equipment refers to the ability of the equipment to withstand the thermal, electromagnetic, electrochemical or other effects of the electrical currents which might be expected to flow when the equipment is part of a system. These currents include, for example, load currents, transient overloads, fault currents, pulses of current and, for alternating current circuits, currents at various power factors and frequencies. Insulation must be effective to enable the equipment to withstand the applied voltage and any likely transient over-voltages.
	A knowledge of the electrical specification and the tests, usually based on the requirements of national or international standards, will assist the user in identifying the withstand properties of the equipment so that it may be selected and installed to comply with this regulation. Such tests are normally carried out either by the manufacturer or by an accredited testing organisation.
	The strength and capability of electrical equipment is not necessarily the same as its rating. Usually the rating is that which has been assigned by the manufacturer following a number of agreed tests.
	Electrical equipment should be used within the manufacturer's rating (continuous, intermittent or fault rating as appropriate) and in accordance with any instructions supplied with the equipment.
	So that equipment remains safe under prospective fault conditions, you must select equipment that takes account of the fault levels and the characteristics of the electrical protection which has been provided for the purpose of interrupting or reducing fault current (excess current protection is required by regulation 11). Most electrical equipment will be able to withstand short-circuit currents safely for limited periods only. The considerations also extend to conductors and equipment provided solely for protective purposes, eg earthing conductors must be adequately rated to survive beyond fault clearance times to ensure satisfactory protective gear operation and fault clearance.
Regulation 11	
Clause 167	The defence (regulation 29) is available in any proceedings for an offence under this regulation (see paragraphs 177–179).
	It is recognised that faults and overloads may occur on electrical systems. The regulation requires that systems and parts of systems be protected against the effects of short circuits and overloads if these would result in currents which would otherwise result in danger.
	The means of protection is likely to be in the form of fuses or circuit breakers controlled by relays etc, or it may be provided by some other means capable of interrupting the current or reducing it to a safe value.
	 When selecting the means of protection, you must consider a number of factors – the more important of these include: (a) the nature of the circuits and type of equipment to be protected; (b) the short-circuit energy available in the supply (the fault level); (c) the nature of the environment; (d) whether the system is earthed or not.

AND GUIDANCE		
	su div	ne circuits to be dealt with may vary from high-power, high-voltage circuits, eg for the inter-connection of substations or for the apply to large motors, down to the smallest final circuit supplying a few low-power lamps at, say, 6 V. Over this range lies a great versity of equipment, each item of which will possess characteristics which must be carefully considered in the selection of popopriate devices to protect against excess current.
	sur	ne maximum short-circuit current in the protected circuit must be considered. (The ability of circuit breakers and fuses to operate iccessfully and without dangerous effects, serious arcing or, in the case of oil-filled equipment, the liberation of oil, is implicit in the quirements of regulations 4 and 5.) The design of the protective arrangement must also provide for sufficient current to be railable to operate the protective devices correctly in respect of all likely faults.
	Clause 177 Th	ne defence (regulation 29) is available in any proceedings for an offence under this regulation.
	Clause 178 In If a pro cu	some circumstances it will be technically impossible to achieve total compliance with the absolute requirement to prevent danger. an excess of current is drawn due to a fault or overload, eg due to an arcing fault, then whatever form of electrical protection is ovided, there will be some danger at the point of the fault during the finite time taken for the detection and interruption of the fault irrent. Nevertheless, electrical protection – whether by means of a simple fuse or another method – must be properly chosen and stalled in accordance with good electrical engineering practice. The protection must be efficient and effective.
	Regulation 12	
	co su	ne need for means to cut off the supply and effect isolation depends on factors such as likely danger in normal and abnormal onditions. This assessment may be influenced by environmental conditions and provisions to be made in case of emergencies, ich as a fire in premises. It includes consideration of which electrical equipment could be a source of danger if such means were of provided and of the installation, commissioning, operational and maintenance requirements over the life of the equipment.
	Regulation 29	
	rea	egulation 29 applies only in criminal proceedings. It provides a defence for a dutyholder who can establish that they took all asonable steps and exercised all due diligence to avoid committing an offence under regulations 4(4), 5, 8, 9, 10, 11, 12, 13, 14, 5 or 16.
HSG85 2013		quipment must be properly designed, constructed, installed and maintained so that it does not present a risk of electric shock, urns, fire or explosion when properly used.
	inc fac rec	bu must select equipment that is suitable for the environment in which it is used, for example cables and equipment in heavy dustries such as sheet metal works need to be protected against mechanical damage. You should consider adverse environmental ctors when working on equipment. For example, excessively damp or humid conditions will increase the risk of injury because of duced effectiveness of insulation, which may undermine the effectiveness of devices used for isolation, or increase the severity hould an electric shock occur. Equipment that has corroded may not function as intended.

IND GUIDANCE	
ESQC Regulations	Regulation 3, Generators, distributors and meter operators shall ensure that their equipment is: (1) (a) sufficient for the purposes for and the circumstances in which it is used; and (b) so constructed, installed, protected (both electrically and mechanically), used and maintained as to prevent danger, interference with or interruption of supply, so far as is reasonably practicable.
	Regulation 4 Generators, distributors, suppliers and meter operators shall: (a) disclose such information to each other as might reasonably be required in order to ensure compliance with these Regulations; and (b) otherwise co-operate amongst themselves so far as is necessary in order to ensure compliance with these Regulations.
	Regulation 6 A generator or distributor shall be responsible for the application of such protective devices to his network as will, so far as is reasonably practicable, prevent any current, including any leakage to earth, from flowing in any part of his network for such a perio that that part of his network can no longer carry that current without danger.
	Regulation A distributor shall ensure that his network shall be: 23, (1) (a) so arranged; and (b) so provided, where necessary, with fuses or automatic switching devices, appropriately located and set, as to restrict, so far as is reasonably practicable, the number of consumers affected by any fault in his network.
	 Regulation A distributor or meter operator shall ensure that each item of his equipment which is on a consumer's premises but which is not 24, (1) under the control of the consumer (whether forming part of the consumer's installation or not) is: (a) suitable for its purpose; (b) installed and, so far as is reasonably practicable, maintained so as to prevent danger; and (c) protected by a suitable fusible cut-out or circuit breaker which is situated as close as is reasonably practicable to the supply terminals.
	 Regulation A distributor shall provide, in respect of any existing or proposed consumer's installation which is connected or is to be connected to 28 his network, to any person who can show a reasonable cause for requiring the information, a written statement of— (a) the maximum prospective short circuit current at the supply terminals; (b) for low voltage connections, the maximum earth loop impedance of the earth fault path outside the installation; (c) the type and rating of the distributor's protective device or devices nearest to the supply terminals; (d) the type of earthing system applicable to the connection; and (e) the information specified in regulation 27(1), which apply, or will apply, to that installation.